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Superconducting Parametric Amplifiers

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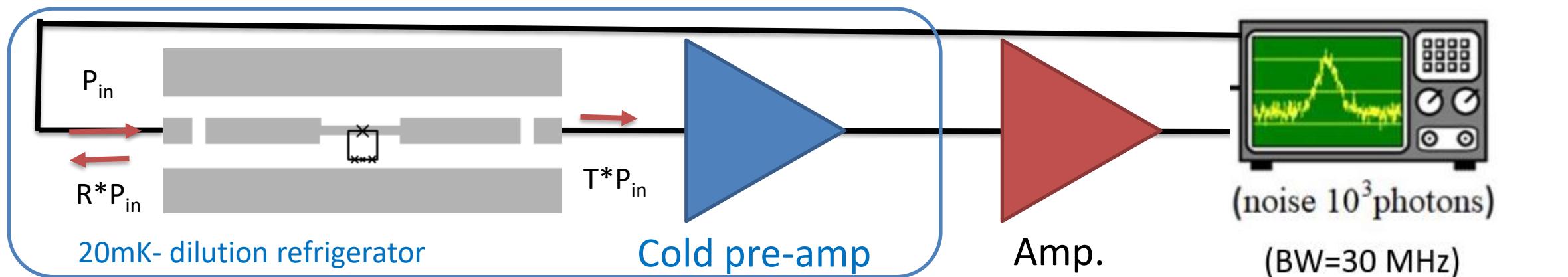
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Experimental requirements for QC

- Circuit QED - qubit state probed by microwave signal - R,T
- Qubit energy $\Delta/h \sim 6 \text{ GHz} = 300 \text{ mK}$, for high coherence $hf \gg k_b T \rightarrow T < 50 \text{ mK}$
- High-Fidelity Readout $n_{\text{cav}} \leq 10$ (\sim expected photons over time 1/BW in the amp.)

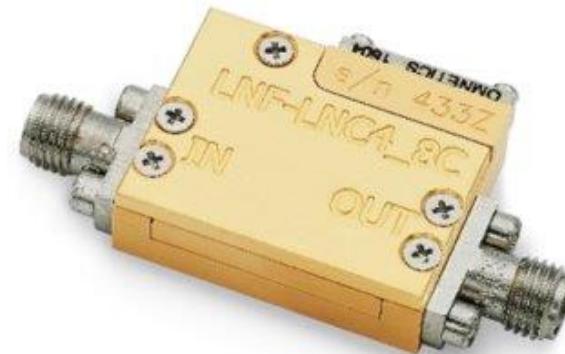
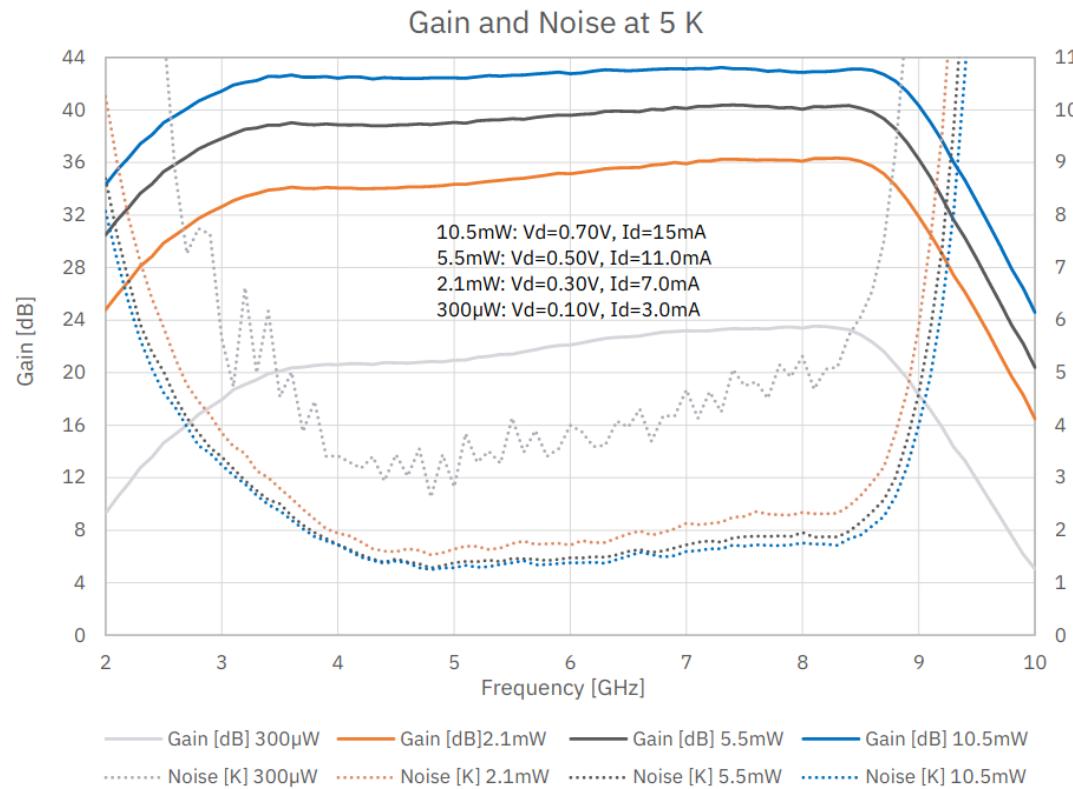
Quantum system, few photon signal



- Amplifier, T_N equivalent noise temperature - white noise of $R=50\Omega$; $N_{\text{out}}=G^*(N_{\text{in}}+k_b T_N)$
- High signal to noise ratio /low noise temperature is critical! Cryogenic amplifier.

Cryogenic HEMT amplifiers

- Advantages: Broadband, high gain, flat gain profile, reliable, easy to use, high dynamic range, provide isolation, commercially available



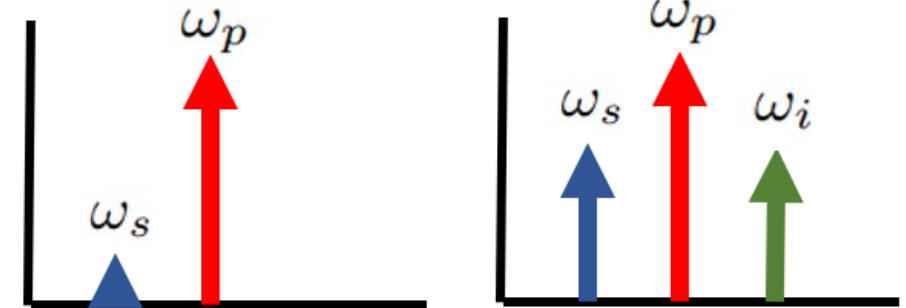
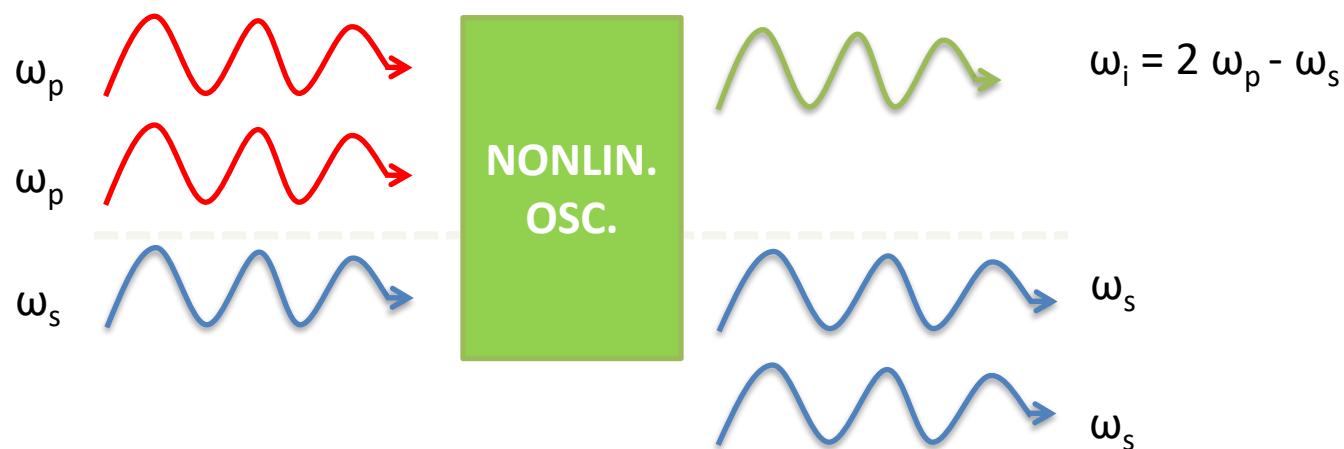
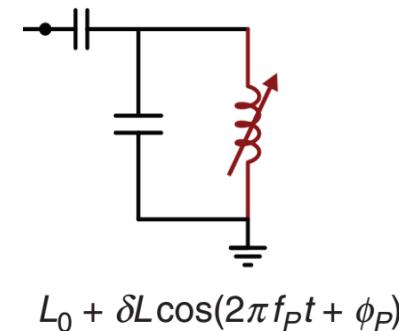
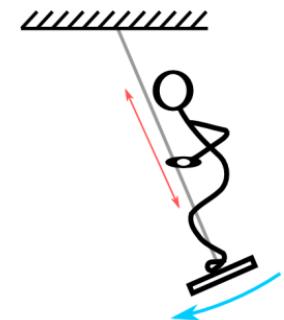
RF Bandwidth	4-8 GHz
Noise Temperature	1.5-2 K
Gain	42 dB
Power dissipation	10 mW

https://lownoisefactory.com/product/lnf-lnc4_8c/

- Disadvantages: Minimum operation temperature 3-4K, high dissipation ~10mW, noise temperature 2 K → $n_{\text{HEMT}} \sim 10$ photons

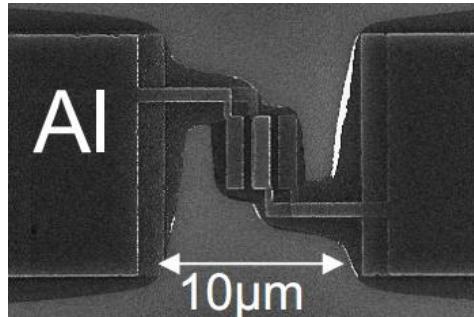
Parametric amplification

- Driven oscillator with a modulated system parameter – energy transfer between modes
 - Child on a swing - resonance frequency ω_0 modulated (pumped) at $2\omega_0$
- LC resonator with variable inductance – nonlinear inductance
- 4 wave mixing – photon model: $\omega_p + \omega_p = \omega_s + \omega_i$

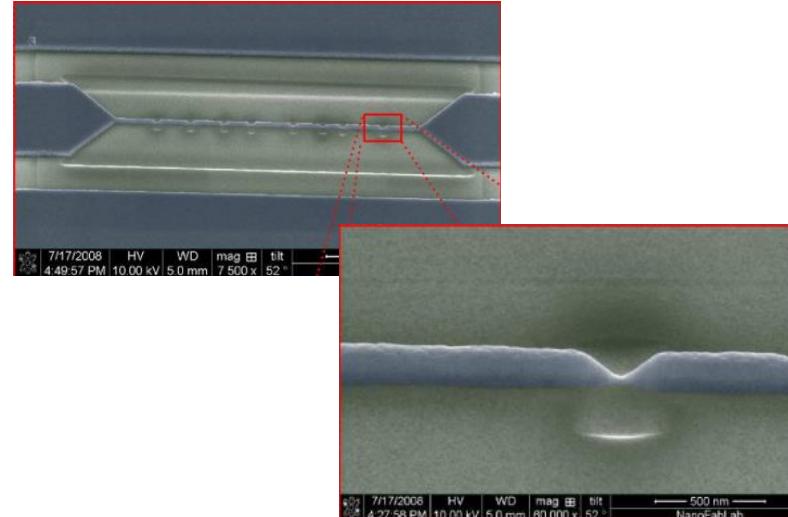


Superconducting parametric amplifiers

- Nonlinearity – nonlinear inductance
 - Josephson Junctions and SQUIDs
 - Disordered superconductors - High kinetic inductance



$$L(I) = \frac{\Phi_0}{2\pi I_0 \sqrt{1 - (I/I_0)^2}}$$



E. A. Tholén et al 2009 Phys. Scr. 2009 014019

Parametric amplification by coupled flux qubits

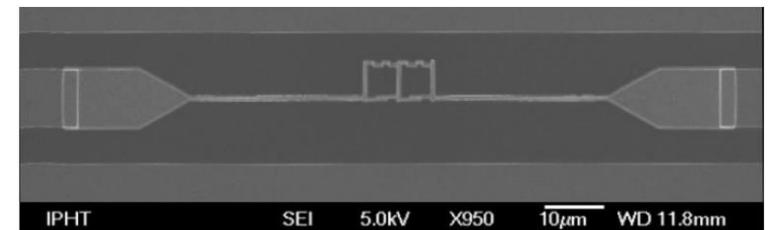
M. Rehák,^{1,2} P. Neilinger,^{1,2} M. Grajcar,^{1,2} G. Oelsner,³ U. Hübner,³ E. Il'ichev,^{3,4} and H.-G. Meyer³

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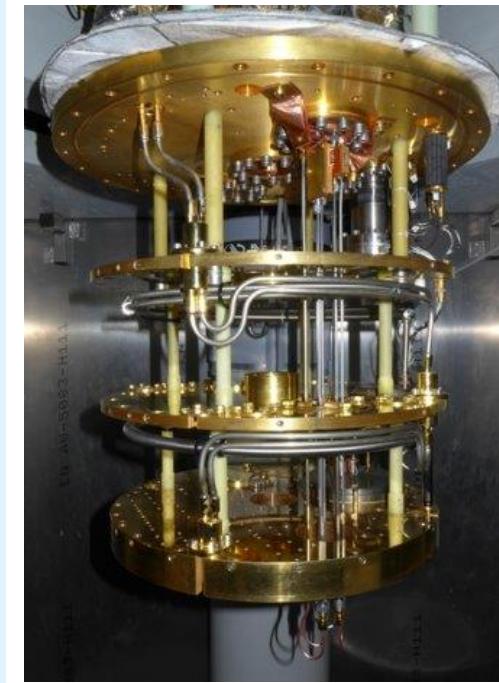
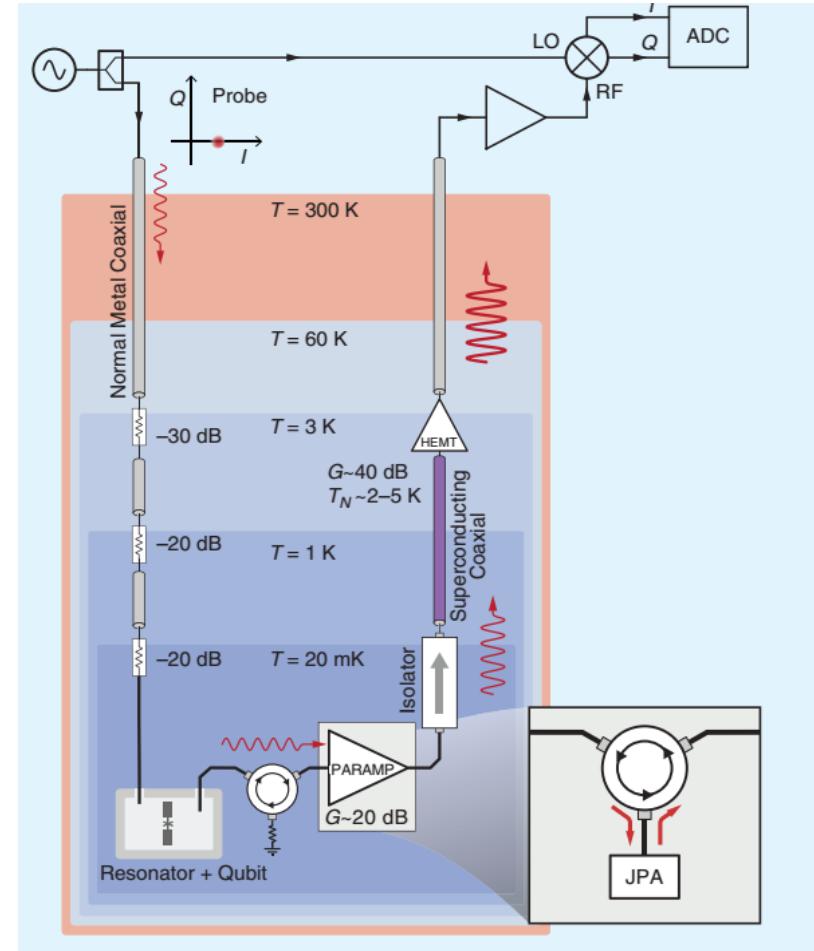
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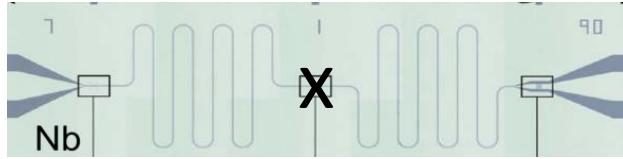
Experimental set-up for QM with ParAmps

- $^3\text{He}/^4\text{He}$ dilution refrigerator
- Paramps work at 20 mK
- Superconducting ParAmps have no dissipative elements
- Quantum limited amplifier
 - Added-noise number number $n_N^{\text{SQL}} = 1/2$
- Advantages: High gain, ultra-low noise, low power dissipation
- Superconducting ParAmps are an **enabling** technology for superconducting qubit measurement



Superconducting parametric amplifiers

- Resonant parametric amplifiers

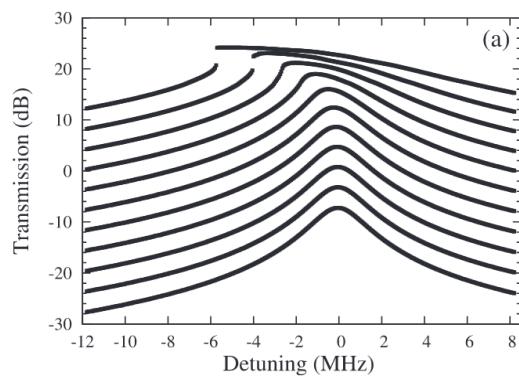


- Duffing oscillator

$$\ddot{y} + \delta\dot{y} + \alpha y + \beta y^3 = F_p \cos(\omega_p t)$$

$$y_p = P \cos(\omega_p t - \phi_p)$$

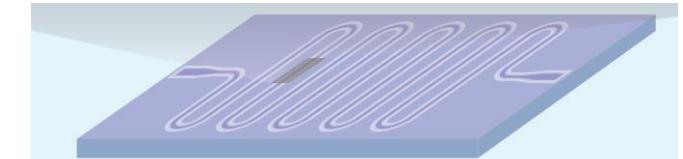
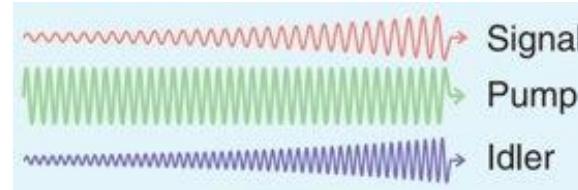
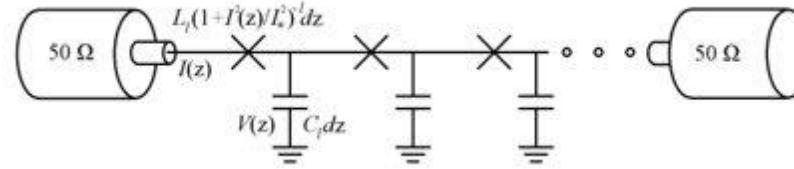
$$P = \frac{F_p}{\sqrt{(\omega_p^2 - \alpha - \frac{3}{4}\beta P^2)^2 + (\delta\omega_p)^2}}$$



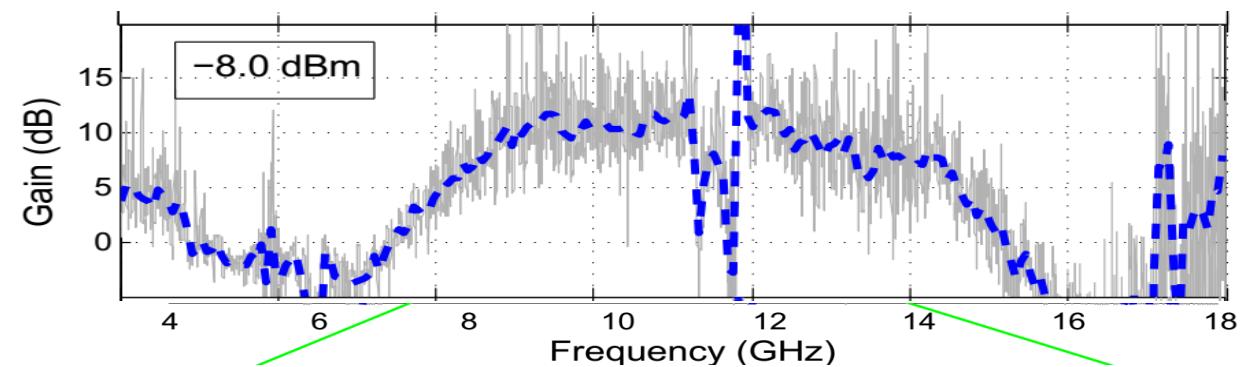
- + SQL noise and below (squeezing), high gain
- Limited bandwidth ~ 1 MHz

- Broadband amplifiers – traveling wave parametric amplifiers (TWPs)

- Long nonlinear waveguide, array of JJs \rightarrow Wave-mixing



J. Aumentado, IEEE Microwave Magazine 21(8):45-59 (2020)



- + Broadband - several GHz

- Gain ripples, demanding fabrication, higher noise

B. H. Eom et al., Nature Physics 8, 623–627 (2012)

Coupled mode theory

- Current in waveguide

$$I(x, t) = \sum_{j \in \{p, s, i\}} \frac{1}{2} \left(I_j(x) e^{i(k_j x - \omega_j t)} + c.c. \right)$$

- Telegrapher's equation for nonlinear medium

$$\frac{\partial^2 I(z, t)}{\partial z^2} - L_l C_l \frac{\partial^2 I(z, t)}{\partial t^2} = \frac{L_l C_l}{6 I_c^2} \frac{\partial^2 I(z, t)^3}{\partial t^2}$$

...

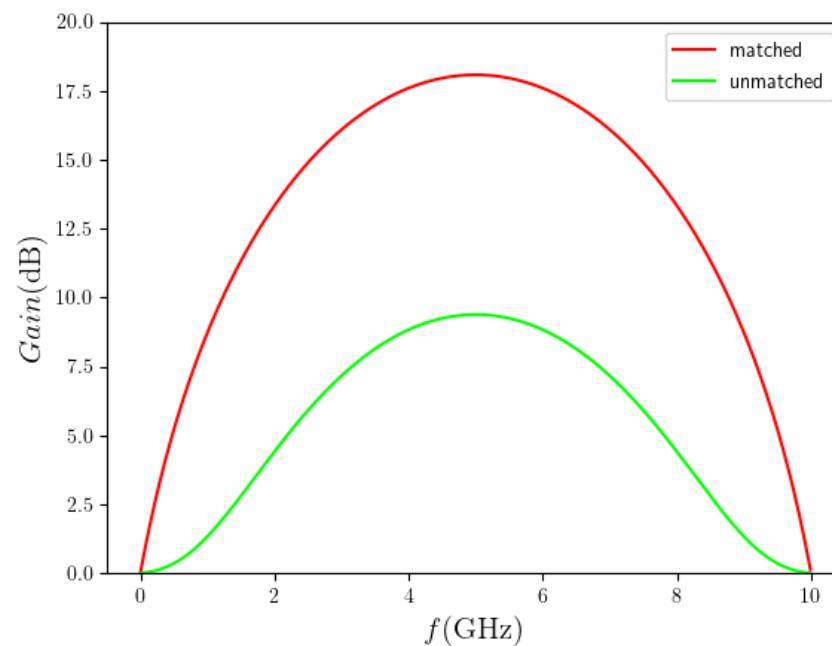
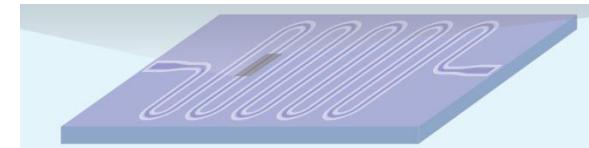
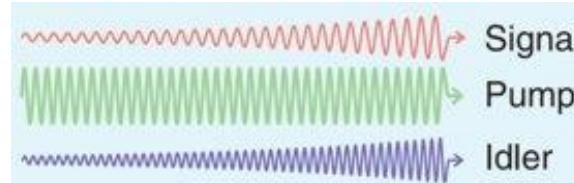
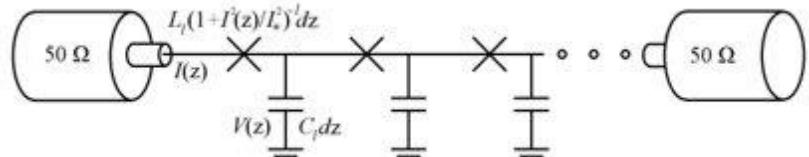
Gain:

$$g = \sqrt{k_s k_i \gamma^2 - \frac{\beta^2}{4}}$$

Phase mismatch: $\beta = \Delta k(1 + 2\gamma) - 2k_p \gamma$

$$\Delta k = 2k_p - k_s - k_i$$

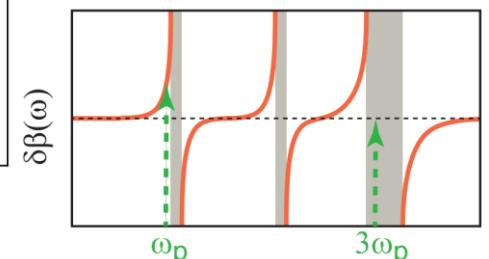
Nonlinearity strength: $\gamma = \frac{|t_p I_p|^2}{16 I_c^2}$



Unmatched phase $\beta \neq 0$:
 $G \sim I^2$

Matched phase $\beta=0$:
 $G \sim \exp(I)$

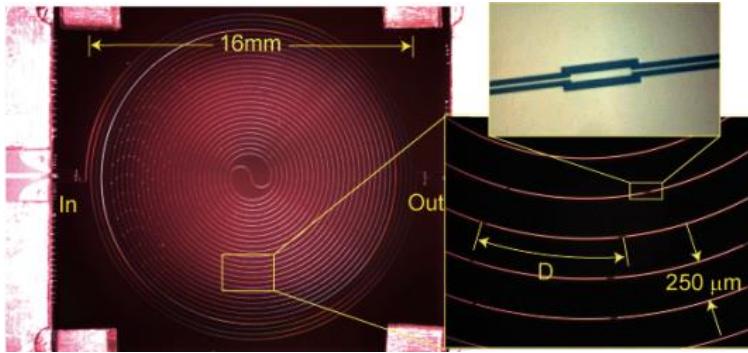
Dispersion engineering



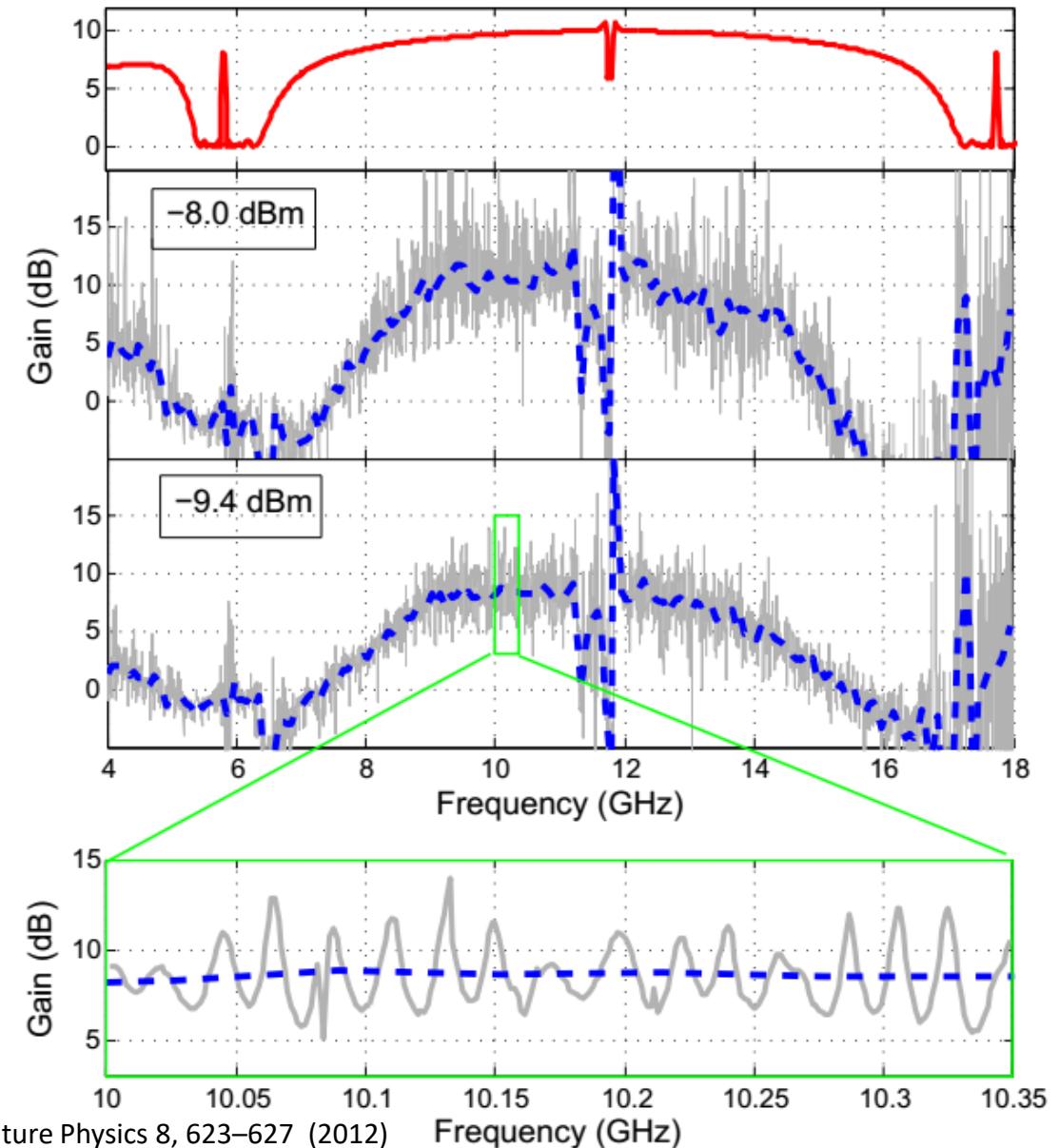
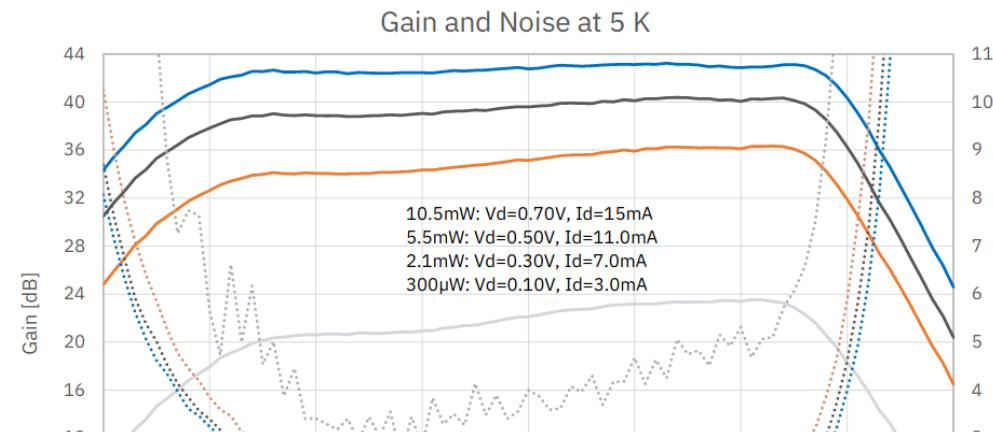
Fixed pump frequency

Coupled mode theory vs experiment

- 80 cm nonlinear waveguide, Impedance $Z=200 \Omega$



- Phase matched – high gain
- Strong ripples - limits the usability of TWPA
- Coupled mode theory fail to explain the ripples



Coupled mode theory with reflections

- Current in finite waveguide with unmatched impedance

$$I(x, t) = \sum_j^{\{p,s,i\}} \frac{1}{2} \left(I_j(x) t_j (e^{ik_j x} + \Gamma e^{-ik_j x}) e^{-i\omega t} + c.c. \right)$$

$$\frac{\partial^2 I(z, t)}{\partial z^2} - L_l C_l \frac{\partial^2 I(z, t)}{\partial t^2} = \frac{L_l C_l}{6 I_c^2} \frac{\partial^2 I(z, t)^3}{\partial t^2}$$

Gain: $g = \sqrt{k_s k_i \gamma^2 (1 + 4|\Gamma|^2)} - \frac{\beta}{4}$

Phase mismatch:

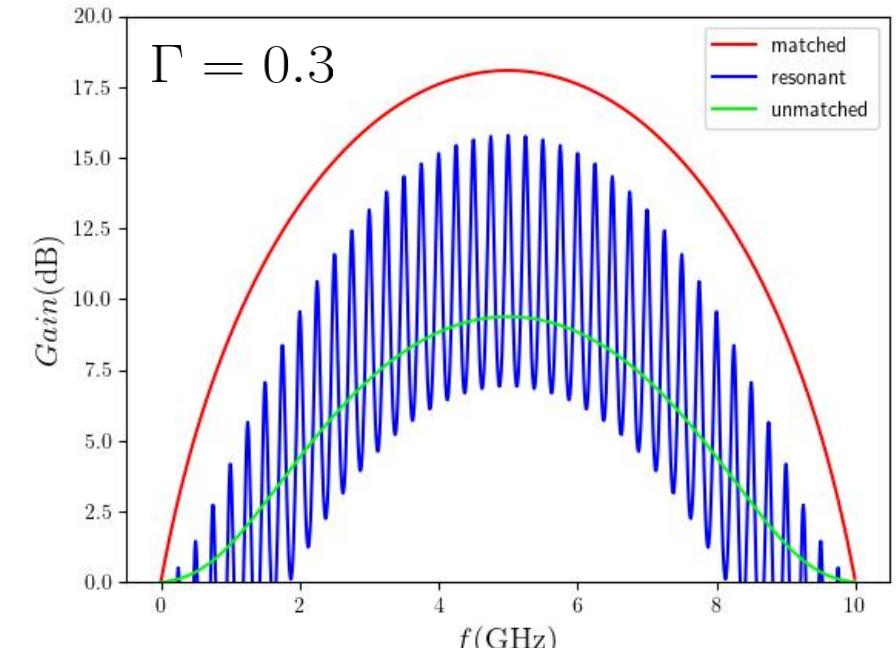
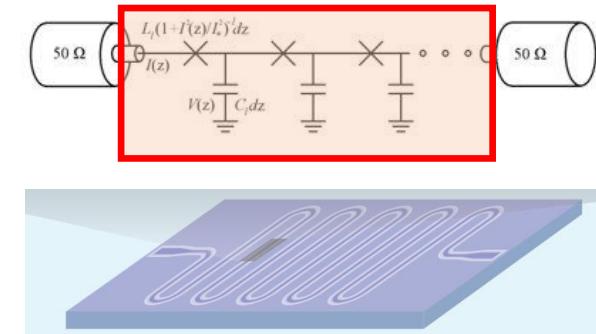
$$\beta = \Delta k (1 + 2\gamma(1 + \Gamma^2)) - 2k_p \gamma (1 - \Gamma^2)$$

Nonlinearity strength: $\gamma = \frac{|t_p I_p|^2}{16 I_c^2}$

- Fabry-Perot resonator

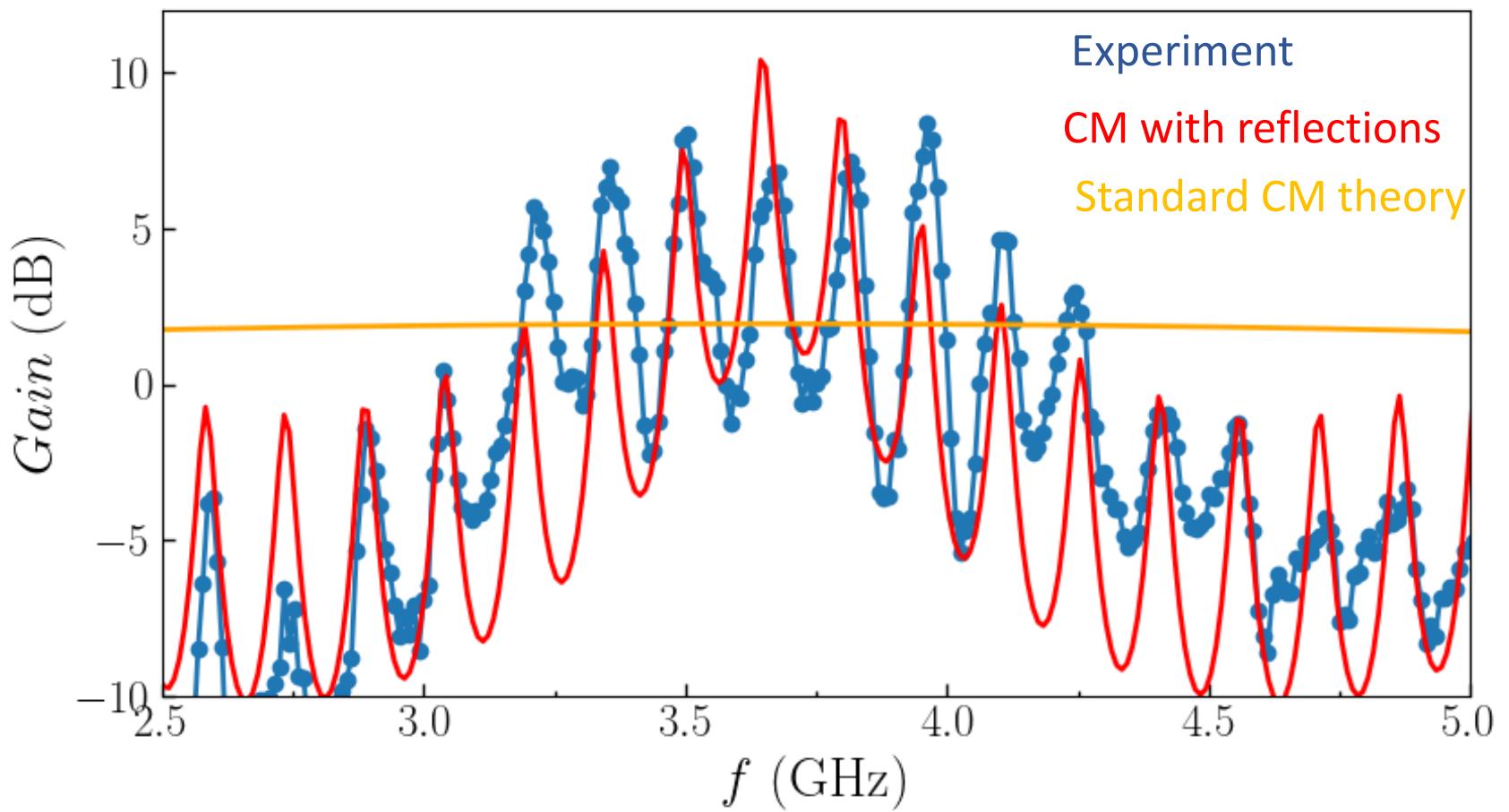
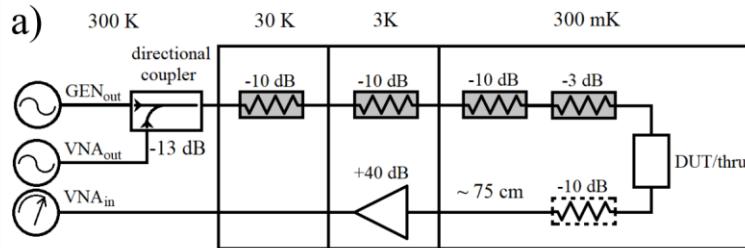
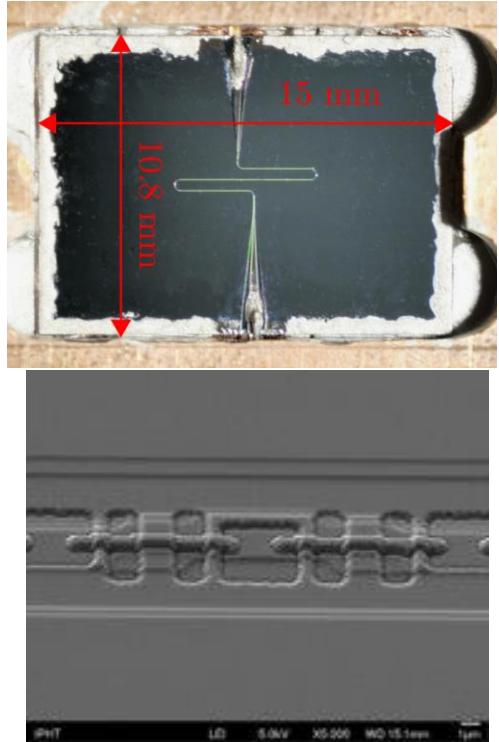
$Z=200 \Omega$

$$\begin{aligned} \Gamma &= \frac{Z - Z_L}{Z + Z_L} \\ t_n &= \frac{1}{1 - \Gamma^2 e^{i2k_j L}} \\ BW &= \frac{\sqrt{1 - \Gamma^2}}{\Gamma} \frac{v}{4\pi l} \end{aligned}$$



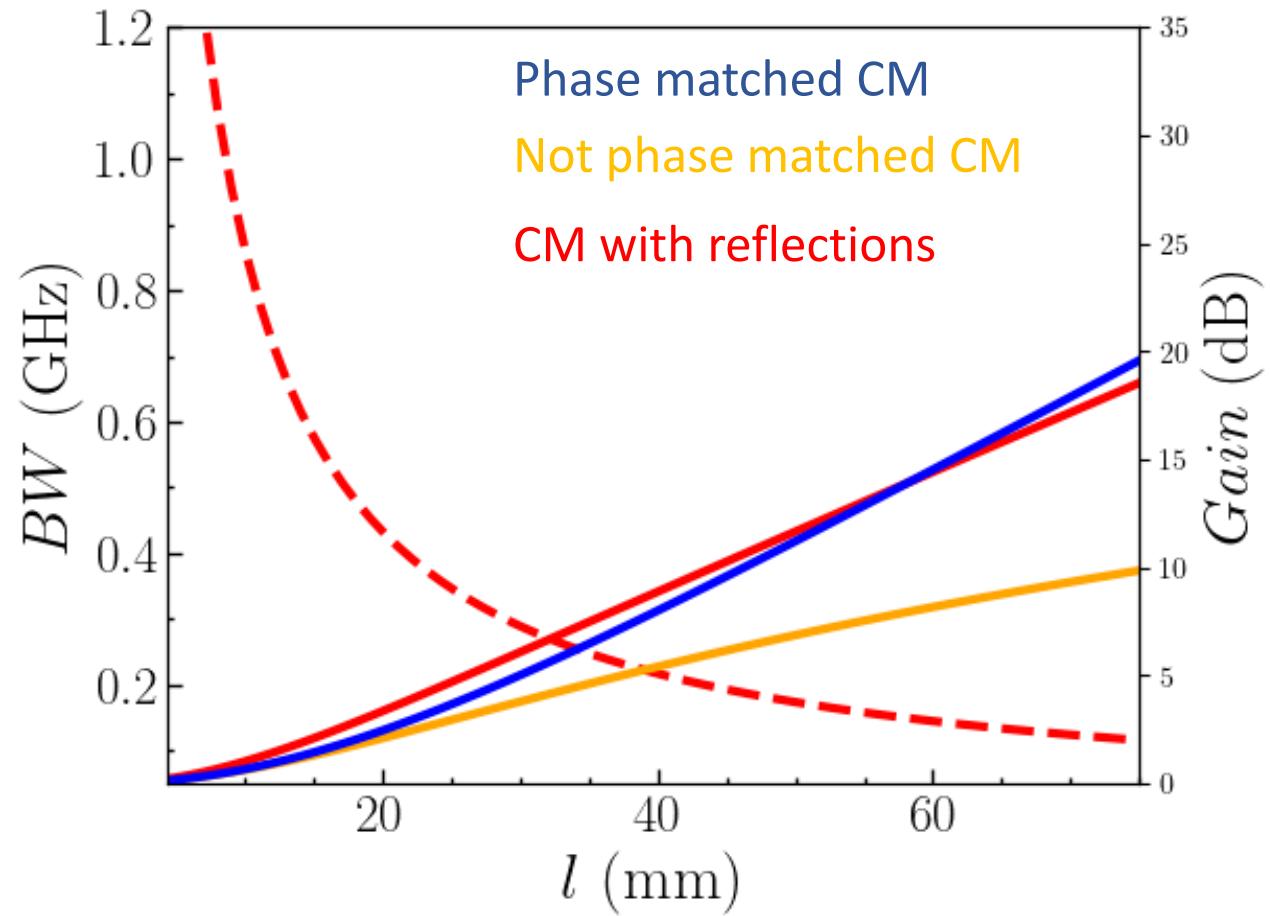
Nb JJ TWPA - experiment

- Array of 2000 JJ in coplanar waveguide, $l=11\text{mm}$, $v_{ph} = 0.14c$, tested at $T = 3.5\text{K}$



Conclusion

- Modified CM theory
 - unmatched TWPA with finite length
- Proper understanding of gain ripples and amplifier bandwidth
- Can be utilized in TWPA design
- The transition regime between traveling-wave and resonant parametric amplifier
- Gain 10dB at 11 mm length without phase matching
 $BW \sim 100\text{MHz}$, – tunable design



Thank you for your attention!

S. Kern, et al. arXiv:2203.02448 (2022)

